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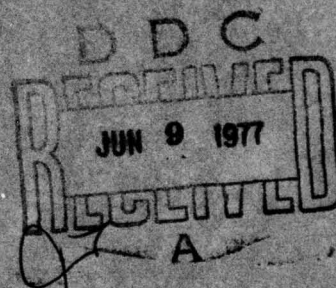
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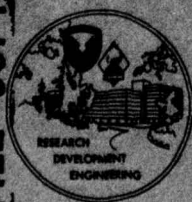
Response of LWIR HgCdTe Photoconductive
Detectors to Ionizing Radiation

December 1976

TR-1768-Response of LWIR HgCdTe Photoconductive Detectors to Ionizing Radiation- by Stewart Shure



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originate from Compton interactions in the surrounding material--for example, glass dewar external to the detector. Initial decay characteristics of the detector response following a prompt gamma pulse appear to depend on the detector material, proceeding either through a bimolecular or a Shockley-Read recombination process. At longer times following the pulse, trap-limited processes become operative in which the fractional level of decay eventually reaches the same value for all the material-preparation techniques evaluated in this work. This applies to detectors in which the surface was left untreated, or was passivated. A detector with the surface treated with a ZnS antireflection coating, however, exhibited an enhanced long time decay response at the largest gamma doses.

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1. INTRODUCTION

Infrared sensing elements are being used or are under consideration for use in a wide variety of system applications including guidance, fuzing, and surveillance. In addition to being sensitive to optical radiation, they are also expected to be sensitive to high-energy ionizing radiation, such as would be encountered in a hostile nuclear environment. Because many systems are required to maintain operation in such environments, it is necessary to know and to be able to predict the effect of nuclear radiation on optical detectors.

This report discusses the effect of ionizing radiation on long wavelength infrared (LWIR) HgCdTe photoconductive optical detectors. A variety of effects, detrimental to system operation, can result when the detector is placed in such an environment. From a system standpoint, for example, a low-level background can produce false signals which, in turn, can result in a system misfiring, a high-level background can degrade system sensitivity below specification, and a transient pulse can cause the system to be "off the air" for an extended time interval. These effects will be modeled and then applied to experimental data taken on representative commercial HgCdTe devices.

2. FACILITIES

The low- and high-level radiation background experiments were performed at the 39 kCi ^{60}Co air source located at the Armed Forces Radiobiological Research Institute. By varying the distance between the source and the detector, gamma fields were obtained with dose rates ranging from 1 to 220 rads/s at the detector. The dose rate was measured actively with an air ionization chamber and a digital readout.

Transient pulse experiments--that is, prompt gamma--were performed at the High Intensity Flash X-Ray (HIFX) located at the Harry Diamond Laboratories. Dosimetry was accomplished by CaF thermoluminescent dosimeters (TLD's) and a Victoreen TLD reader. The width (FWHM) of the x-ray pulse is 21 ns; the energy spectrum peaks at 2 MeV. Total dose ranged from 0.2 to 360 rads, depending on the distance between the Ta bremsstrahlung target and the detector.

3. PREIRRADIATION DEVICE DATA

Four different detectors were studied. Two of them were supplied by Honeywell Radiation Center and denoted HRC and HRC #8, one was supplied by Arthur D. Little, Inc. and denoted ADL, and one was supplied by Aeronutronic Ford Corp. and denoted AF.

Table I lists several device parameters, including device area (A), device thickness (d), extrinsic carrier concentration (n_o), detector resistance between the contacts (R), peak detector responsivity (R_λ) at 12- μ m wavelength at a bias (V_B), and the condition of the surface. All the samples were n-type. The carrier concentrations are known to approximately ± 20 percent, except for the ADL device which is known only approximately within a factor of 2. All the detector areas were square,

TABLE I. PHOTODETECTOR DATA

Detector	A (cm ²)	d (cm)	n_o (cm ⁻³)	R (Ω)	$R_\lambda V_B$ (V/W/V)	Surface
HRC	10^{-5}	1.2×10^{-3}	7×10^{14}	54	1.3×10^5 1.1	ZnS
ADL	6.25×10^{-4}	1.2×10^{-3}	2.5×10^{14}	140	840 1.4	Untreated
AF	4.5×10^{-3}	2.5×10^{-3}	8.0×10^{14}	90	750 1.45	Pass
HRC #8	6.25×10^{-4}	1.2×10^{-3}	10^{15}	25	1800 1.25	Untreated

except for the AF device which was 0.175 by 0.025 cm. The detectors were mounted in LN₂ dewars enabling them to be operated at 77°K. All the detectors were designed to have a wavelength cutoff of $\lambda_{co} = 13$ to 14 μ m, which is equivalent to an alloy concentration of approximately 20 percent Cd, that is, Hg_{0.80}Cd_{0.20}Te.

The AF detector material used for fabricating the units was supplied by Cominco, Inc. The material was grown by a process similar to the slush-recrystallization technique developed by Harman.¹ The detector was epoxy-mounted on a sapphire substrate which was, in turn, epoxy-mounted on a No. 42 alloy. A passivation coating was deposited over the detector. There was no ZnS antireflection coating. The dewar window was Ge with an antireflection coating. The ADL detector material was grown in a high-pressure furnace² by an open ampoule technique that allowed impurities--for example, Cl, O, N, and H--to boil off. The detector was mounted on an IRTRAN II substrate (ZnS) and was in optical contact (that is, not air spaced) to a Ge immersion lens. The dewar window was IRTRAN II. The detector surface was untreated--that is, no passivation or ZnS antireflection coating. The Honeywell detectors were grown in a Bridgman Furnace³ by a closed ampoule technique. Two detectors were studied. One (HRC) was mounted on a ZnS substrate and had a ZnS antireflective coating on the detector and an IRTRAN II dewar window. The other was mounted on a sapphire substrate and also had a Ge dewar window. The detector surface was left untreated.

¹T. C. Harman, *J. Electronic Mat.*, 1, (1972). p. 230.

²J. Steininger, *Proceedings of Meeting of IRIS Specialty Group on IR Detectors* (13-15 March 1973) p. 33.

³P. W. Kruse, *Appl. Optics*, 4 (1965), p. 687.

4. EXPERIMENTAL PROCEDURE

Following a prompt gamma pulse, the recovery of the detector was recorded with a Tektronix 7844 oscilloscope and 7A13 and 7A22 differential plug-ins. The peak of the response was measured by the 7A13 plug-in with a 5-MHz bandwidth. The decay of the response was obtained by using the 7A22 with a high-frequency cutoff set at 1 MHz and a low-frequency cutoff set at 1 Hz. This plug-in has a 15-V overload capability down to the lowest gain sensitivities used (1 mV/cm) with overload recovery of the plug-in rated at less than 10 μ s. For the maximum voltages (peak) measured on this experiment (~ 200 mV), the plug-in was not driven into saturation. Figure 1 shows the bias circuit. To reduce the rf pickup from the HIFX pulse so that measurements could be made at times immediately following the pulse, it was necessary to double shield the detector and all leads in addition to using the differential plug-in. The oscilloscope, which was terminated at 50 Ω , and the bias battery were housed in a metal (shielding) box located outside the exposure room. The bias circuit was placed in close proximity to the detector.

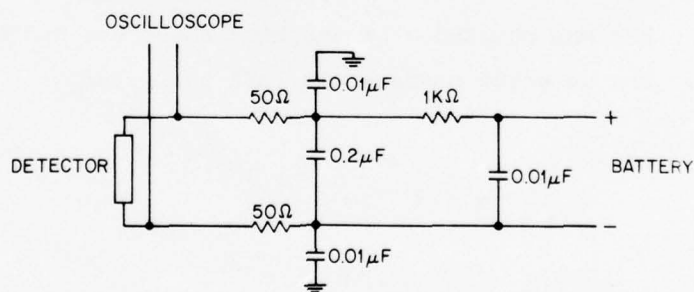


Figure 1. HIFX bias circuit.

The high-level gamma-induced noise measurements were obtained with a Ballentine 320A rms voltmeter, using a 4-MHz bandwidth followed by a 10-MHz-bandwidth amplifier with a gain of 200 placed at the detector input. The detector and amplifier were located in the exposure room and were separated from the measuring apparatus by 30 m. Connections were made with RG-178 cable. The amplifier circuit shown in figure 2 includes a biasing circuit designed to operate at 3-mA detector current.

By replacing the rms voltmeter with a Tektronix 454 oscilloscope and an Ortec counter/scaler, the low-level gamma counting measurements were performed. By using the internal trigger level control, the oscilloscope served as a voltage discriminator. Gamma-induced detector voltage pulses with amplitudes greater than the discrimination level are counted on the counter/scaler via the gate output of the oscilloscope. In this way, the pulse height distribution of the detector noise could be determined.

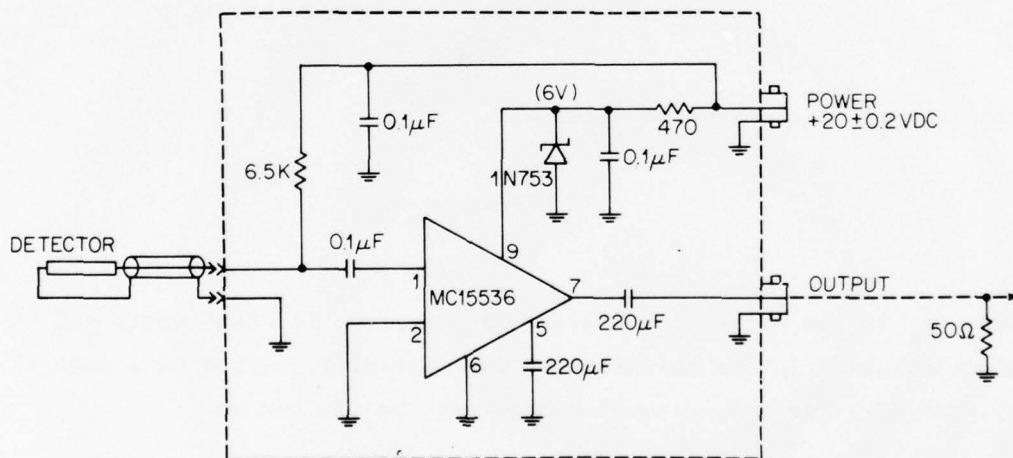


Figure 2. Schematic diagram of 10-MHz preamplifier.

5. THEORY

5.1 Prompt Gamma Pulse

High-energy ionizing radiation incident on a photoconductor generates electron-hole pairs. These give rise to a short circuit photocurrent which can be written as

$$I_s = q\mu V_B \Delta N / \ell^2 . \quad (1)$$

In this equation, q is the charge of an electron, μ is the carrier mobility, V_B is the voltage across the detector, ΔN is the number of carriers generated by the incident radiation, and ℓ is the distance between the current-carrying electrodes. When the load resistor R_L in the bias circuit is greater than detector resistance R_d , the open-circuit voltage V is measured at the detector electrodes; V is given by

$$V = I_s R_d . \quad (2)$$

The detector resistance is given by

$$R_d = \ell / w d q \mu n_o , \quad (3)$$

where n_o is the extrinsic carrier density, w is the width of the detector, and d is the thickness of the detector. From equations (1), (2), and (3), the open-circuit voltage may be written as

$$V = V_B \Delta n / n , \quad (4)$$

where Δn is the density (cm^{-3}) of excess carrier ($\Delta n = \Delta N/wld$) induced by the radiation. The biasing circuits in this experiment (fig. 1 and 2) utilize large load resistors $R_L \gg R_D$; thus, the detector voltage induced by the ionizing radiation is given by equation (4).

In equation (4), Δn is written as

$$\Delta n = 100\rho\dot{D}\tau/\epsilon_\rho, \quad (5)$$

where ρ is the density of the $\text{Hg}_{0.8}\text{Cd}_{0.2}\text{Te}$, \dot{D} is the dose rate in rad/s , τ is the lifetime of the excess carriers, and ϵ_ρ is the electron-hole pair creation energy (in ergs). This expression is valid when the gamma-pulse width is longer than the lifetime. When the lifetime is longer than or equal to the pulse width, equation (5) may be written as

$$\Delta n = 100\rho D/\epsilon_\rho, \quad (6)$$

where D is the dose in the HgCdTe . The value of Δn in equation (6) is for times immediately following the ionizing pulse. At later times, t , after the pulse, the excess carriers decay, to a first approximation, through a single exponential time constant (τ); Δn is given by

$$\Delta n = (100\rho D e^{-t/\tau})/\epsilon_\rho. \quad (7)$$

For low-radiation levels (in equation (4)), n is the initial (electron) doping concentration n_0 . As the radiation level increases, the excess carrier concentration Δn becomes comparable in magnitude with n_0 , so that n is written as $n_0 + \Delta n$. Substituting this in equation (4) yields

$$V = V_B \Delta n / (n_0 + \Delta n). \quad (8)$$

From this equation, the detector voltage resulting from an ionizing radiation pulse (induced by the irradiation) saturates at the detector bias voltage. Equations (7) and (8) will be used to analyze the peak detector voltages induced by the prompt gamma pulse.

5.2 Low-Level Gamma Counting

The effect of a high fluence density of ionizing radiation on HgCdTe detectors has been presented in the preceding section. This section considers the effect of individual high-energy gamma photons on the detector.

High-energy photons, such as would be emitted from a ^{60}Co source (1.17 and 1.32 MeV), interact with the detector primarily through secondary Compton electrons that are emitted from collisions of the gammas with material (i.e., glass) surrounding the detector.^{4,5} Passage of the electron through the detector ionizes electron-hole pairs and gives rise to a voltage pulse at the detector. An approximate value of the voltage pulse induced in the detector⁶ is, from equation (4),

$$V_P = V_B N_Y / w \lambda d n_O , \quad (9)$$

where N_Y is the number of electron-hole pairs released by the passage of a Compton electron. Assuming that these electrons pass through the thickness (d) of the detector, N_Y may be approximated by

⁴R. A. Rotolante, R. P. Muroska, and G. E. Keiser, *Radiation Effects in Intrinsic Photodetector Systems (U)*, Honeywell Radiation Center AMMRC CTR 73-46 (December 1973). (SECRET)

⁵J. W. Haffner, Presented at 1975 IEEE, Annual Conference Nuclear and Space Radiation Effects, Poster Session Paper (14-17 July 1975).

⁶Detector Test Program Final Report, Vol. 1, LMSC-B303910, Contract F04701-70-C-0227 (August 1972).

$$N_Y = \frac{dE}{dx} \frac{d}{\epsilon_\rho}, \quad (10)$$

where dE/dx is the ionization loss rate of the high-energy electrons. A value of N_Y , corresponding to passage through the length (l) and width (w), can be obtained by the appropriate substitutions. However, the probability for such an event is small compared with passage through the thickness.

Calculation of the complete pulse-height distribution requires an involved computer formulation.⁷ However, a rather good closed form expression can be obtained by considering the isotropic interaction of Compton electrons originating in the surrounding material with the detector.⁵ By using an approximate expression for the Compton cross section, an expression for the number of voltage pulses per second out of the detector greater than or equal to a threshold value (P) can be written

$$\begin{aligned} \text{counts/s}(\geq P) = C_6 \Big\{ \exp \left[-(C_2 + C_7) \sin \sqrt{1 - (kd/P)^2} \right] \left[\frac{\sin \sqrt{1 - (kd/P)^2}}{(C_2 + C_7)} \right. \right. \\ \left. \left. + \frac{1}{(C_2 + C_7)^2} \right] - \exp \left[-(C_2 + C_7) \sin \theta_{\max} \right] \right. \\ \left. \left[\frac{\sin \theta_{\max}}{C_2 + C_7} + \frac{1}{(C_2 + C_7)} \right] \right\}. \quad (11) \end{aligned}$$

⁵J. W. Haffner, Presented at 1975 IEEE, Annual Conference Nuclear and Space Radiation Effects, Poster Session Paper (14-17 July 1975).

⁷J. C. Pickel and M. D. Petroff, IEEE Trans. Nucl. Sci., NS-22, No. 6 (1975), p. 2456.

The literal coefficients are

$$C_6 = 2\pi A N_1 \dot{\gamma} C_1 C_5$$

$$C_1 = 1.6 E_{\gamma} + \frac{1.4}{E_{\gamma}^{0.2}} \cdot 10^{-25}$$

$$C_2 = 1 + 1.8 E_{\gamma}$$

$$C_5 = \gamma_1 \left(\frac{E_{\gamma}^2}{0.25 + E_{\gamma}} \right)^{n_1}$$

$$C_7 = 6 \times 10^{-3} (2 + E_{\gamma})^{n_1}$$

$$k = v_B \left(\frac{dE}{dx} \right) / \epsilon_{\rho} n_o l w d$$

$$\theta_{\max} = \cos^{-1} \left[\frac{d}{\delta_1} \left(\frac{E_{\gamma} - 1.02}{2} \right)^{-n_1} \right]$$

where

A = detector area,

N_1 = density of electrons in the surrounding cover,

$\dot{\gamma}$ = incident gamma photon flux,

$E_{\gamma} = 1.25$ Mev (^{60}Co energy),

n_1 and δ_1 are parameters in the range-energy ($R-E_e$) relationship:

$$R \approx \delta_1 (E_e)^{n_1} \text{ where } n_1 = 5/3, \delta_1 = 0.27 \text{ cm}.$$

The values of $C_1 = 3.3 \times 10^{-25} \text{ cm}^2/\text{e}$, $C_2 = 3.25 \text{ cm}^2/\text{e}$, $C_5 = 0.27 \text{ cm}$, and $C_7 = 3.25 \times 10^{-2} \text{ cm}$. This expression applies to electrons that do not stop in the detector.

5.3 High-Level Gamma Noise

An expression for the gamma-induced noise may be obtained by analogy from background-induced generation-recombination (G-R) noise and by approximating the pulse-height distribution by an exponential (consistent with observation). The rms noise voltage from the incident gammas⁶ is

$$V_Y = 2\tau V_P \sqrt{2E_R B}$$
$$B = 1/2\pi\tau, \quad \text{if } \Delta f \leq 1/2\pi\tau \quad (12)$$
$$B = \Delta f, \quad \text{if } \Delta f > 1/2\pi\tau,$$

where V_P is given by equation (9), Δf is the voltmeter bandwidth, and E_R is the event rate; thus,

$$E_R = K\mu\dot{\gamma}wld. \quad (13)$$

In this equation, μ is the linear absorption coefficient of high-energy gammas in HgCdTe, $\dot{\gamma}$ is the incident photon flux (number of gamma photons/cm²·s), wld is the detector volume, and K is a constant that accounts for the effect of secondary Compton electrons whose point of origination is external to the detector. K may be calculated with some degree of accuracy as pointed out in the previous section, or it may be obtained empirically from the experimental pulse-height distribution. When $K = 1$, all the pulses originate from Compton events internal to the detector volume.

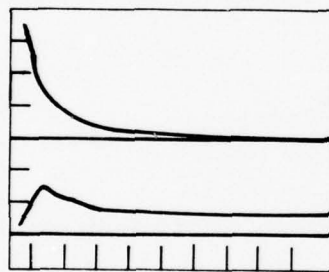
⁶Detector Test Program Final Report, Vol. 1, LMSC-B303910, Contract F04701-70-C-0227 (August 1972).

6. RESULTS

6.1 Prompt Gamma

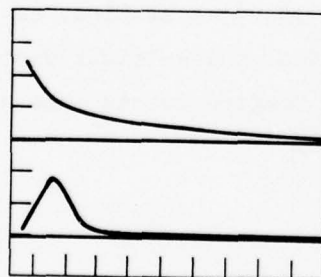
6.1.1 Data

Oscillograms of detector output voltage following a prompt gamma dose in the range of 350 rads for each of the four detectors are given in figures 3 to 6. The lower trace in each figure shows the peak response on the 100-ns/cm time base. The upper trace in each figure shows the decay tail on the appropriate time base down to 2 mV/cm (1 mV/cm for HRC detector) for each detector. The vertical scale readings must be multiplied by 2 to obtain the actual detector output voltages because of 50- Ω termination.



Top trace: 1 mV/cm, 500 μ s/cm
Lower trace: 50 mV/cm, 100 ns/cm
 $V_B = 100$ mV

Figure 3. Response of HRC after 350-rad HIFX prompt gamma pulse.



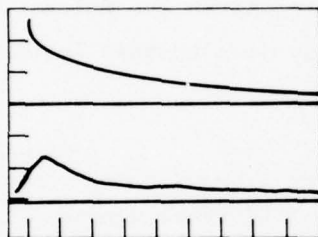
Top trace: 2 mV/cm, 5 μ s/cm
Lower trace: 50 mV/cm, 100 ns/cm
 $V_B = 150$ mV

Figure 4. Response of ADL after 340-rad HIFX prompt gamma pulse.



Top trace: 2 mV/cm, 1 μ s/cm
 Lower trace: 20 mV/cm, 100 ns/cm
 $V_B = 150$ mV

Figure 5. Response of AF after 360-rad HIFX prompt gamma pulse.



Top trace: 2 mV/cm, 2 μ s/cm
 Lower trace: 20 mV/cm, 100 ns/cm
 $V_B = 50$ mV

Figure 6. Response of HRC #8 after 320-rad HIFX prompt gamma pulse.

A few interesting observations have been made about these oscillograms. First, disregarding the different detector biases, the detector designated HRC appears to have a substantially longer decay tail than that of the three other detectors. The HRC #8, AF, and ADL detectors decay to millivolts output between 10 and 20 μ s after the pulse, whereas the HRC detector decays to millivolts on the order of milliseconds after the pulse. This is further demonstrated in figure 7 where V/V_B , the ratio of detector output voltage to detector bias, is plotted versus time after the gamma pulse for the various detectors. It is seen that after scaling the detector voltage by the bias voltage, the detector voltage recovered to 1 percent (0.01) of the bias voltage

at approximately 20 μ s after the pulse for the HRC #8, AF, and ADL detector. The HRC detector recovered to 0.01 in 1 ms. The detector bias voltages, as seen in figure 7, ranged from 50 mV for HRC #8 to 256 mV for AF. Figure 8 gives the detector output voltage of the HRC, AF, and ADL following a 280-rad gamma dose as a function of time after the pulse. The detectors were all biased at 150 mV. Similar recovery times are found for this bias condition as in the preceding case. It was possible to observe the decay of the detector voltage of HRC continuously down to about 0.3-mV detector output. This occurred at 2.5 ms as the oscilloscope trace approached the base line. Because of electrical pickup in the range of 50 to 100 μ s after the pulse, it was not possible to continuously follow the decay down to this level for the

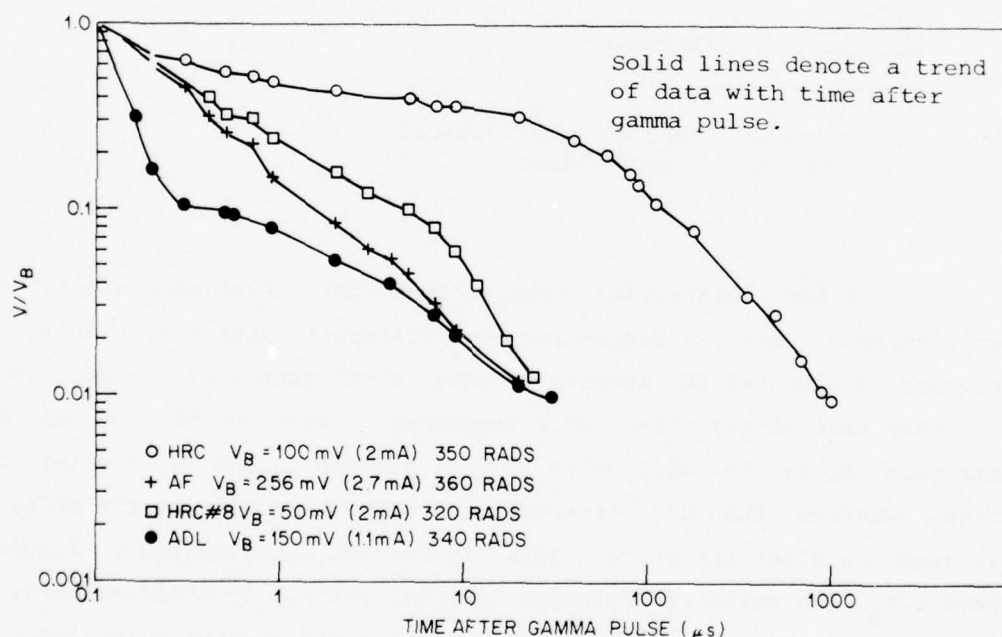


Figure 7. Decay of the detector voltage, scaled by the detector bias voltage, following prompt gamma pulse for the various detectors.

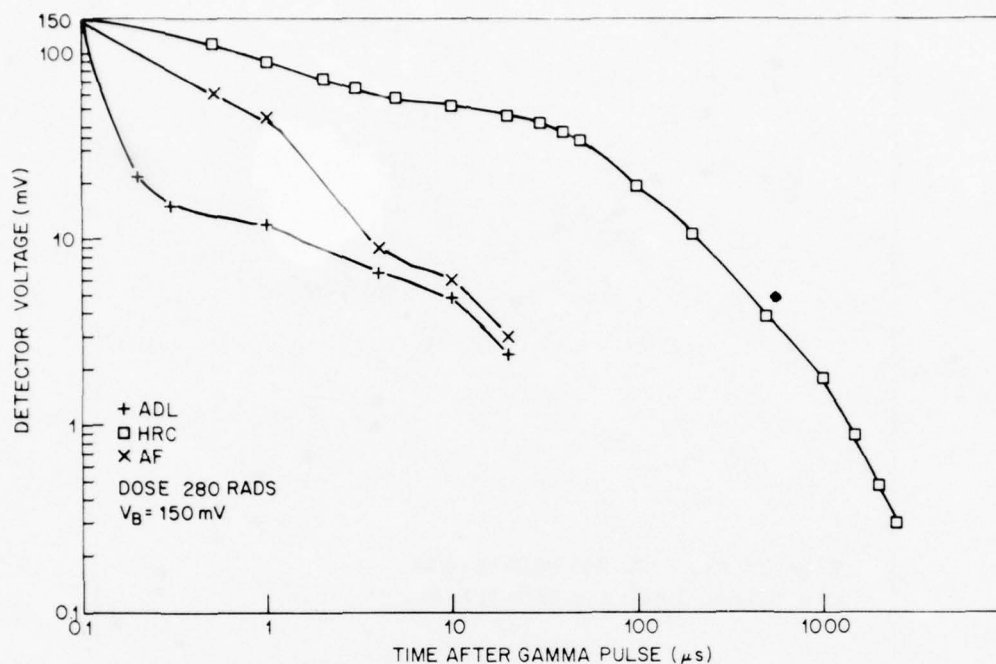


Figure 8. Decay of the detector voltage following the prompt gamma pulse for HRC, AF, and ADL with $V_B = 150$ mV.

ADL, HRC #8, and AF detectors. For prompt doses greater than 100 rads, a zero bias response of the detector was measurable. When this response is subtracted from the peak response with bias, the peak detector voltage is equal to the bias voltage at the highest doses. The effect of detector bias on the decay curve is shown in figure 9, where the response of the AF detector for two bias conditions is given. It is seen that no significant dependence of the decay rate exists on the bias voltage.

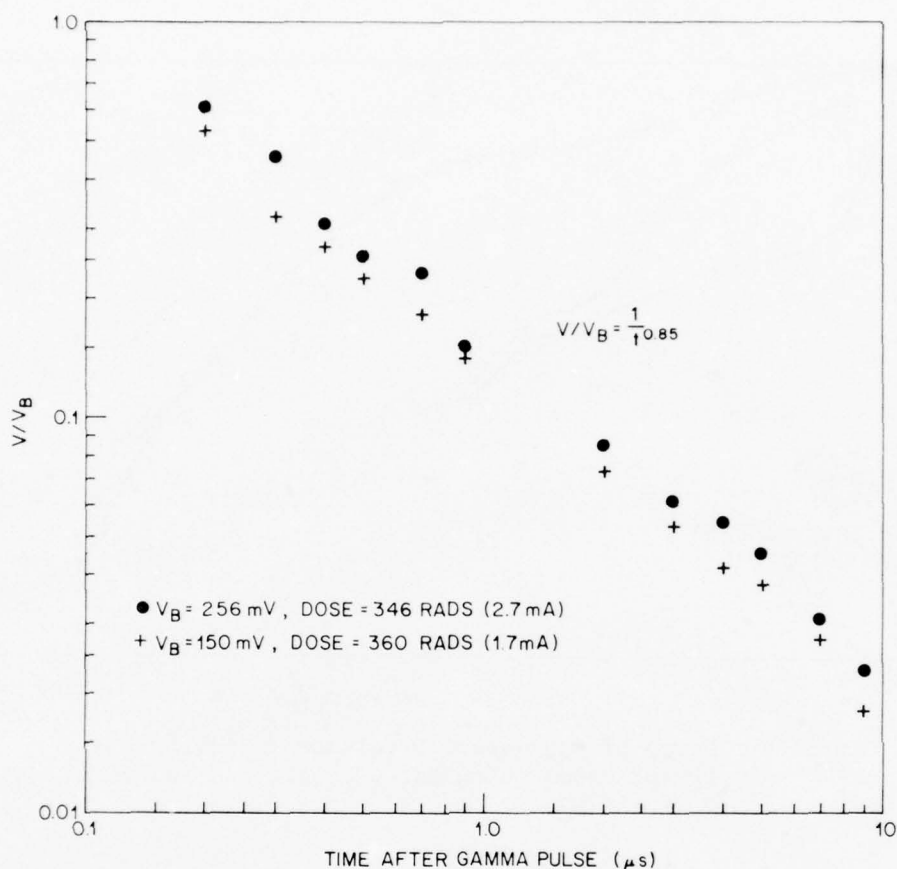


Figure 9. Decay of the detector voltage, scaled by the detector bias, following the prompt gamma pulse for AF with two detector biases, $V_B = 256$ mV and 150 mV.

The dependence of the detector decay on prompt gamma dose is plotted in figures 10 to 12 for HRC, HRC #8, and AF. Here, V/V_B is plotted on semilog paper, versus time (to ~ 1 μs) after the pulse. For HRC the decay tail increases monotonically from a dose-independent initial exponential time constant of 200 ns as the dose increases. The initial decay rate of AF and HRC #8, however, appears to be dependent on

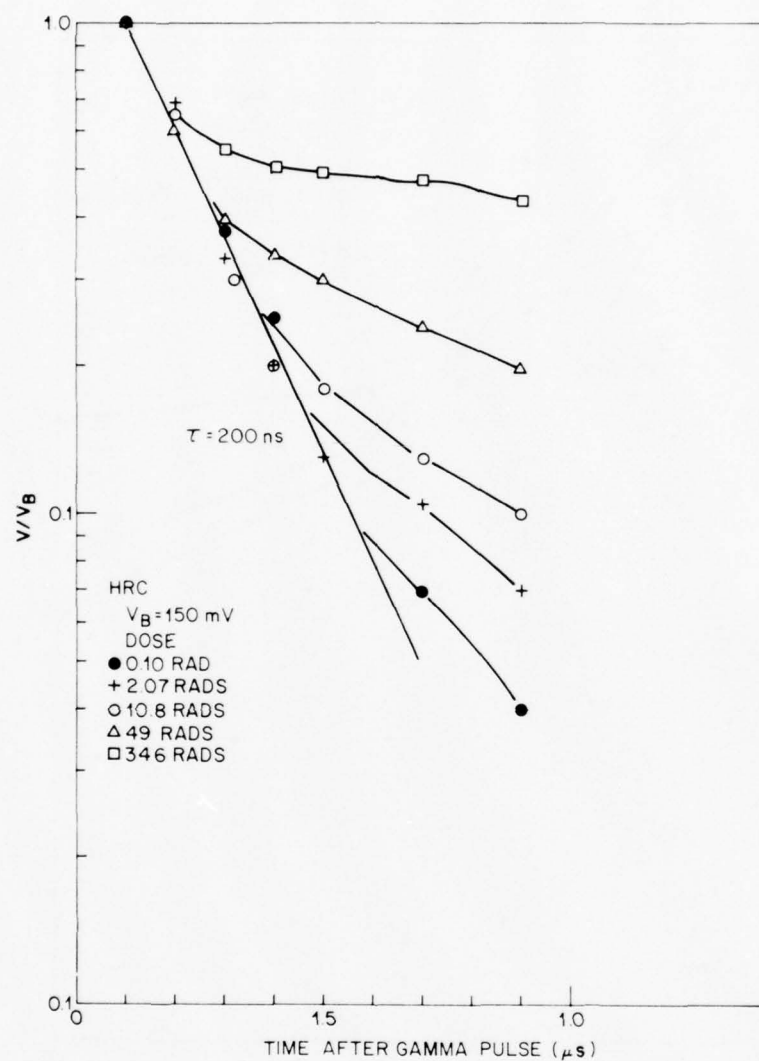


Figure 10. Ratio of detector voltage to detector bias voltage (V/V_B) versus time after the gamma pulse, for HRC with prompt dose as a parameter.

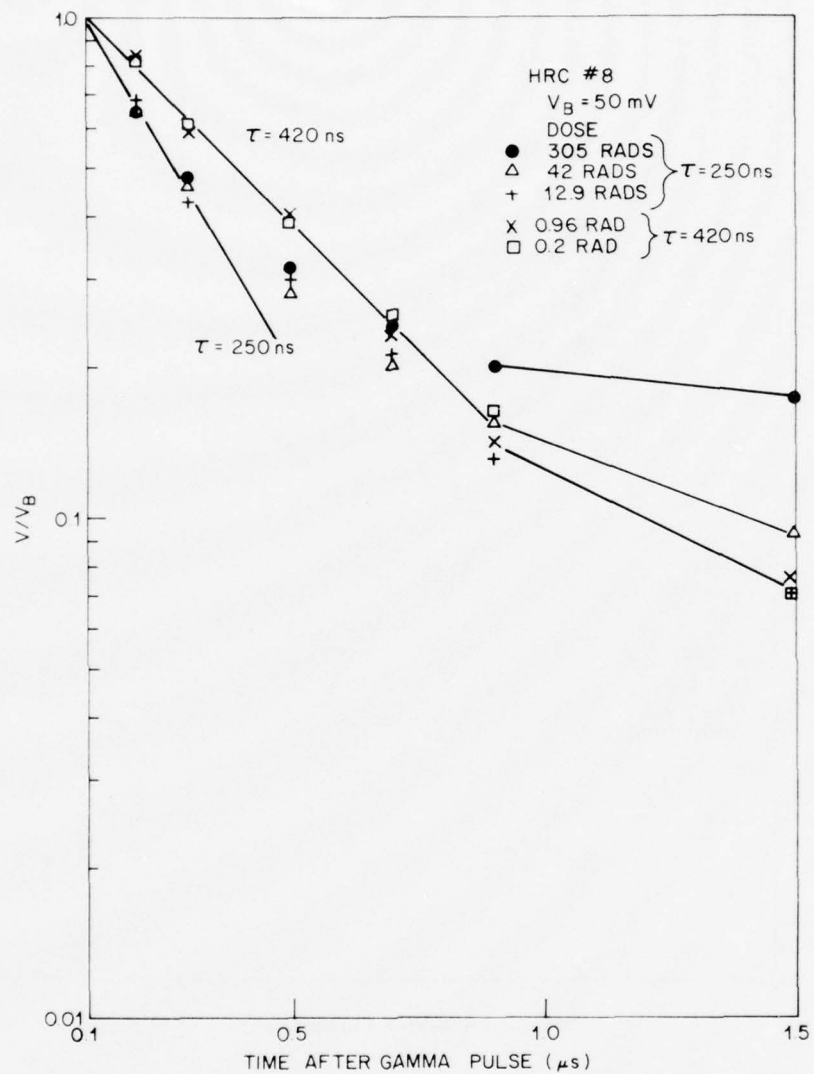


Figure 11. Ratio of detector voltage to detector bias voltage (V/V_B) versus time after the gamma pulse for HRC #8 with prompt dose as a parameter.

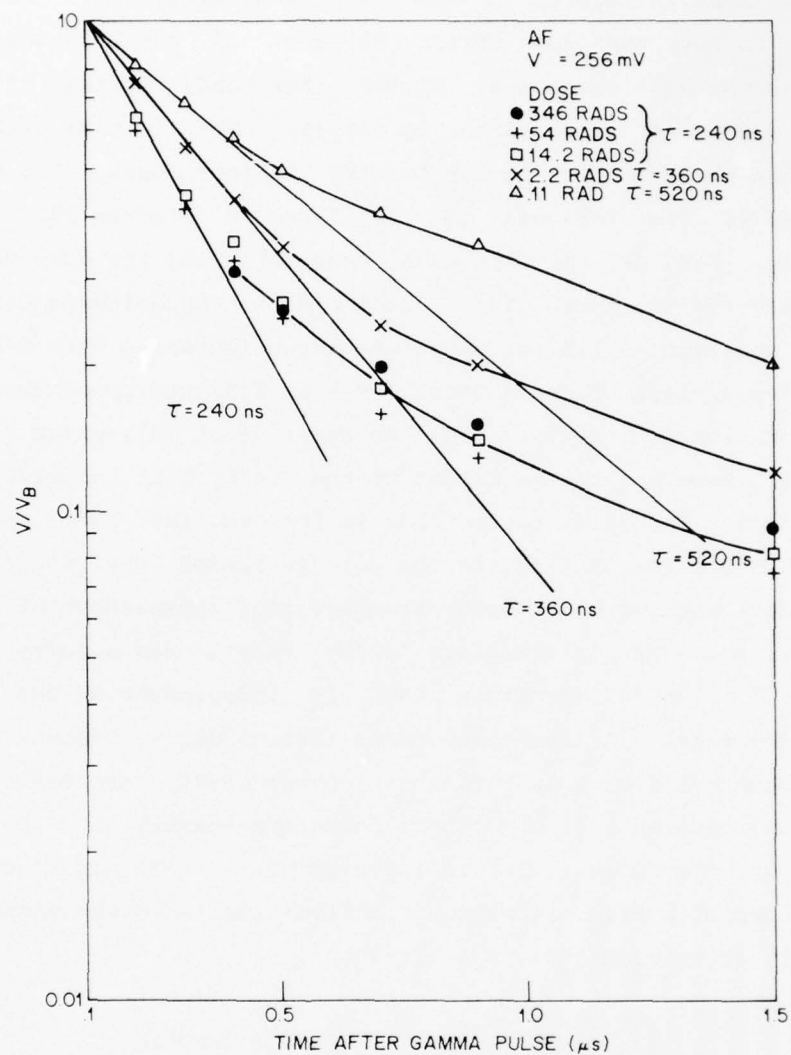


Figure 12. Ratio of detector voltage to detector bias voltage (V/V_B) versus time after the gamma pulse for AF with prompt dose as a parameter.

the dose. As the dose increases, the exponential time constant decreases as seen in figures 11 and 12. The decay tail of HRC #8 appears to follow the same trend as that of the HRC--that is, it increases as the dose increases. On the other hand, the tail of AF (out to 1 μ s) decreases as the dose increases. The initial decay-time constants are given in the figures for the various doses. The decay of AF and HRC #8 are followed out to 7 μ s in figures 13 and 14, respectively. For AF, it is seen that following the dose dependent initial decay region, there is a region with a dose-independent decay rate (time constant is 1.3 μ s) whose magnitude increases with decreasing dose for doses less than 14 rads. This is followed by another region with a yet longer decay time constant (5.5 μ s), which is dose independent. However, the magnitude of the decay tail increases as the dose increases. The decay tail of HRC #8 follows the same dependence, as seen in figure 14; that is, as the dose increases the magnitude of the tail increases with the decay-time constant independent of dose and equal to 5.7 μ s. The intermediate decay region has a decay constant equal to 0.67 μ s and a magnitude that is independent of dose between 12.9 and 305 rads. A dose independent initial decay constant equal to 45 ns was observed for ADL. This is considerably shorter than the initial decay constants of the other detectors--namely 200 to 500 ns, depending on the dose. It is interesting to note that effective optical values of carrier lifetime, τ , calculated⁸ from the equation for responsivity at wavelength λ , R_λ , given by,

$$R_\lambda = \eta(\lambda) \cdot \lambda \cdot \tau \cdot V_B / wld \cdot hc \cdot n_o$$

⁸D. Long and J. L. Schmitt, *Mercury-Cadmium Telluride and Closely Related Alloys, Semiconductors and Semimetals*, Vol. 5, ed. by R. K. Willardson and A. C. Beer, Academic Press, New York (1970), p. 175.

with the data in table I, yield values comparable with the initial lifetimes obtained in the prompt gamma experiment at the lower dose.

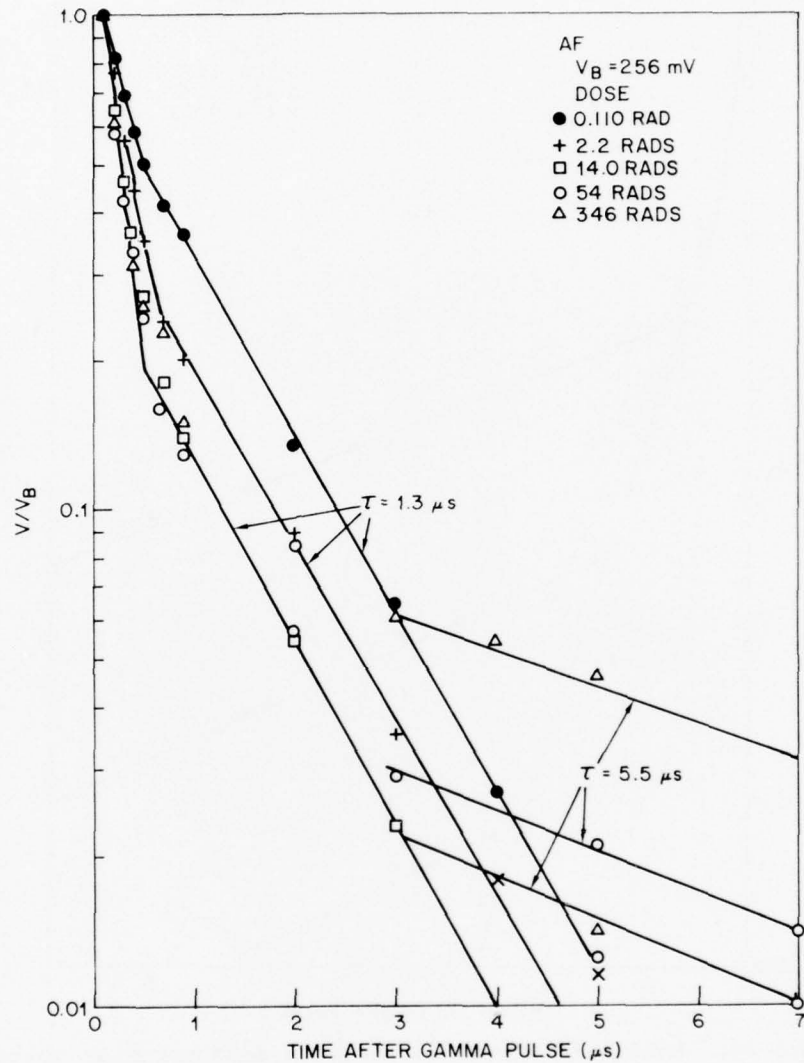


Figure 13. Ratio of detector voltage to detector bias voltage (V/V_B) versus time after the gamma pulse for AF with prompt dose as a parameter.

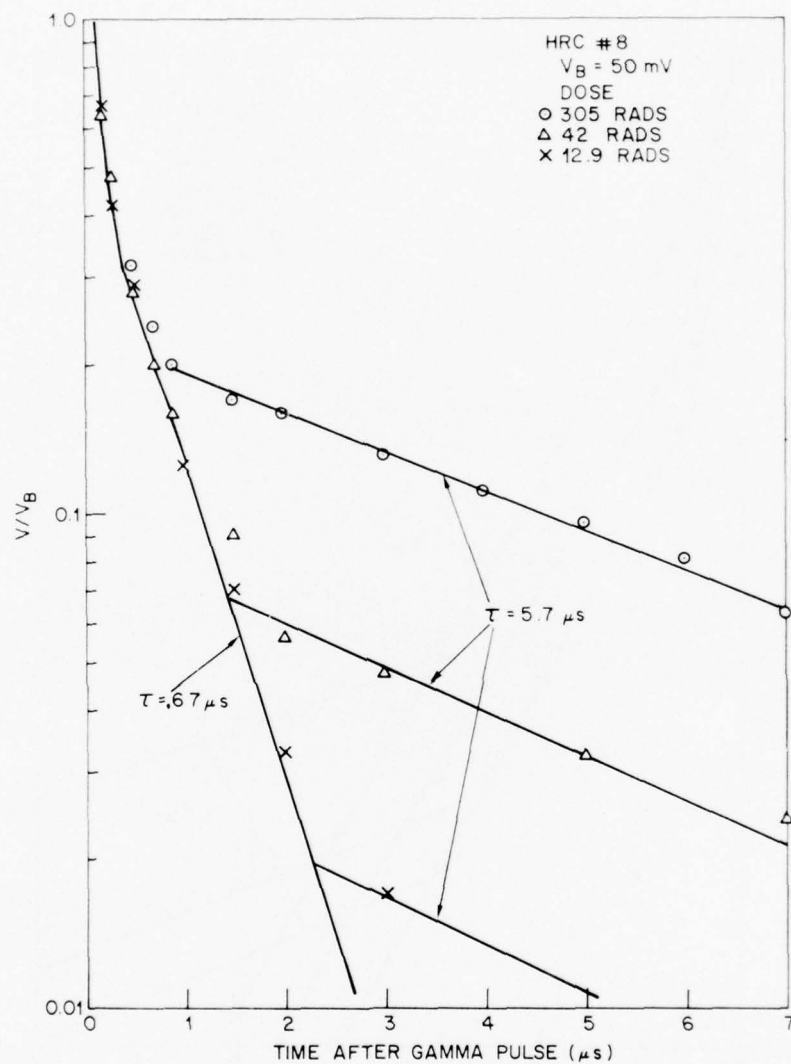


Figure 14. Ratio of detector voltage to detector bias voltage (V/V_B) versus time after gamma pulse for HRC #8 with prompt dose as a parameter.

The effect of prompt gamma dose on the magnitude of peak voltage induced in the detector is given in figures 15 to 18 for the four detectors. The voltage peaks, V_p , which occurred 100 ns after the pulse, were scaled by the bias voltage V_B given in figures 15 to 18. For doses over 100 rads, a zero-bias response was observed, which contributed to the response with bias. When it was subtracted from the biased response, the value of V_p/V_B was unity for all the detectors tested. As seen in figures 15 to 18, all the detectors become saturated for doses in the range of 20 to 40 rads. As the dose decreases below 10 rads the peak voltage decreases. Data taken on the AF detector (fig. 18) show that the peak voltages are not dependent on the detector bias level.

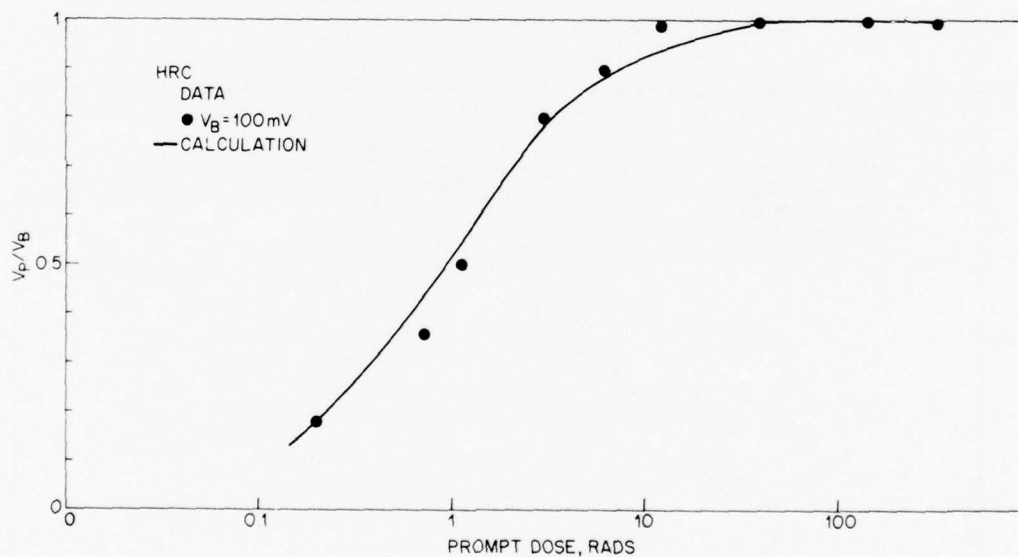


Figure 15. Ratio of peak detector voltage following a prompt gamma pulse to detector bias voltage versus prompt dose for HRC.

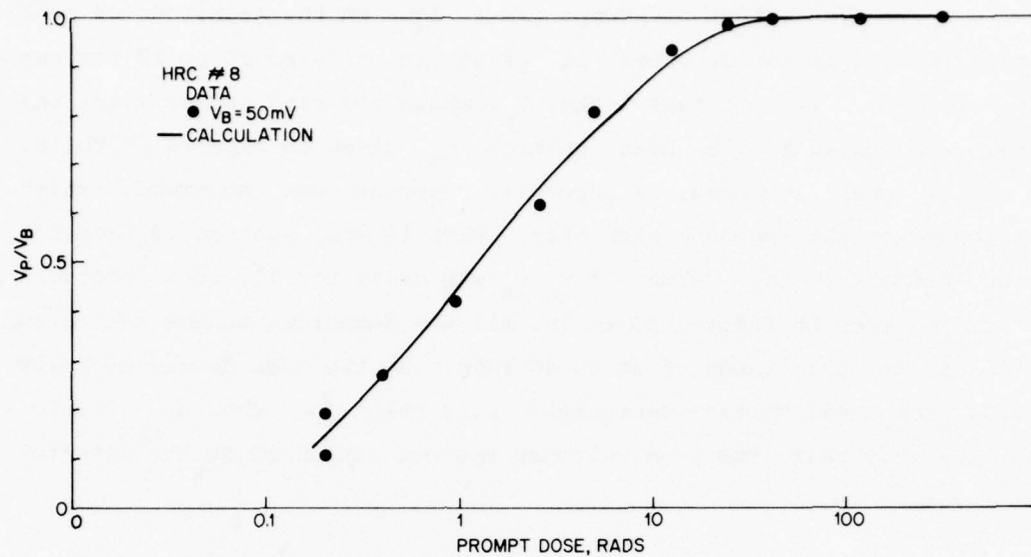


Figure 16. Ratio of peak detector voltage following a prompt gamma pulse to detector bias voltage versus prompt dose for HRC #8.

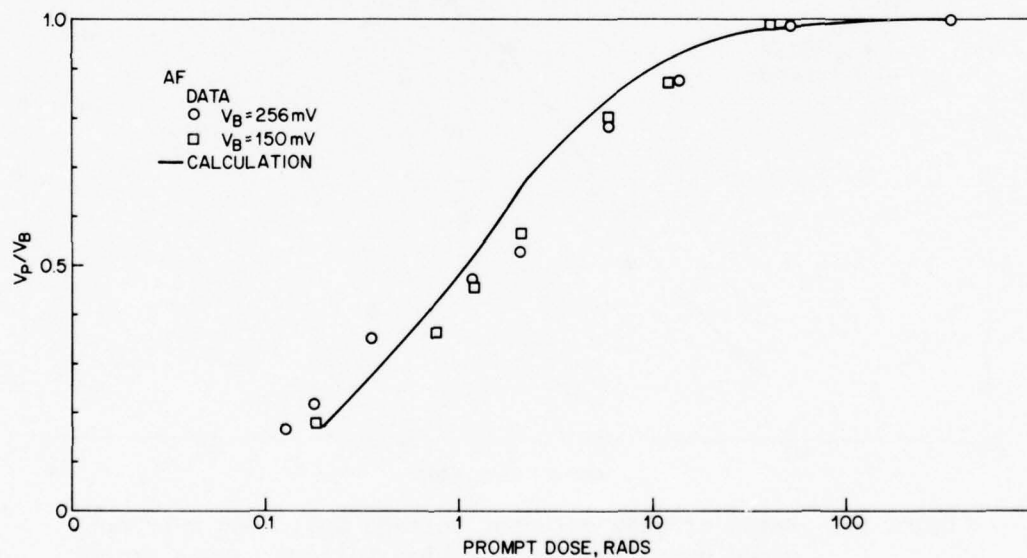


Figure 17. Ratio of peak detector voltage following a prompt gamma pulse to detector bias voltage versus prompt dose for AF.

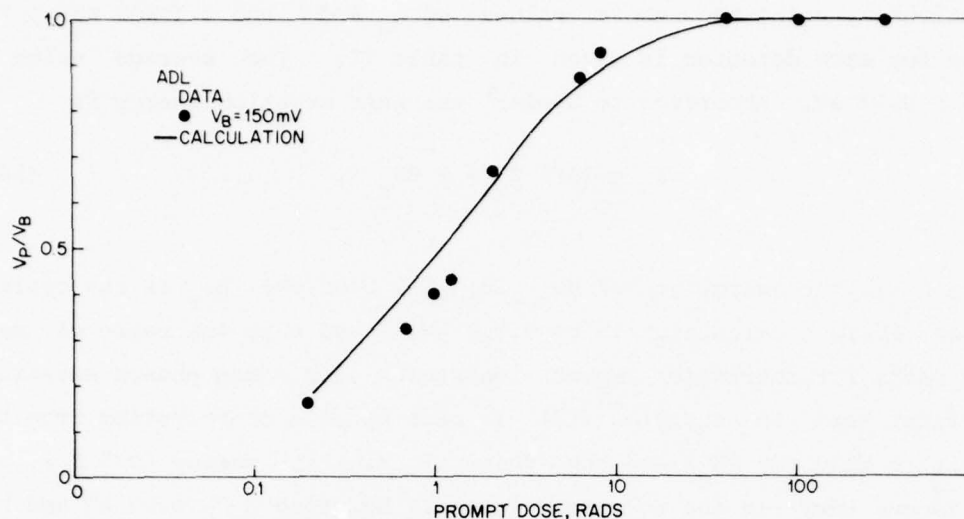


Figure 18. Ratio of peak detector voltage following a prompt gamma pulse to detector bias voltage versus prompt dose for ADL.

6.1.2 Comparison of Theory and Experiments

The dependence of the peak voltage on prompt gamma dose, figures 15 to 18, will be discussed by using equations (7) and (8). Based on these equations, good agreement with data, shown by the solid lines in the figures, can be obtained by using values of n_0 , τ , ϵ_ρ given in table II; n_0 was taken from table I. The values of τ were obtained from the initial exponential decay times following prompt gamma doses. The density of $\text{Hg}_{0.80}\text{Cd}_{0.20}\text{Te}$ is 7.5 g/cm^3 . The value of t in equation (7) was 100 ns, the time after the pulse at which the peak voltage was measured. The electron-hole pair creation energy ϵ_ρ was determined as a parameter by requiring that the data satisfy these

equations by using the above values of n_0 and τ and t ($=100$ ns). The value for each detector is given in table II. The average value is 0.36 ± 0.07 eV. According to Klein,⁹ the pair creation energy is

$$\epsilon_{\rho} = 14/5 E_g + r h\omega_r, \quad (14)$$

where E_g is the energy gap of $\text{Hg}_{0.8}\text{Cd}_{0.2}\text{Te}$, 0.09 eV; $h\omega_r$ is the optical phonon energy calculated to be 0.016 eV,¹⁰ and r is the ratio of mean free paths for intrinsic impact ionization and Raman phonon emission. The first term in equation (14) is made up of a contribution from the intrinsic band gap (E_g) and the residual kinetic energy ($9/5 E_g$), and the second term is due to phonon losses. By using $E_g = 0.09$ eV and $h\omega_r = 0.016$ eV, a value of 0.36 eV is calculated from equation (14) if $r = 7$. This is similar to the value of r ($=8$) for Si.⁹

The decay of photoconductivity after cessation of the excitation pulse may proceed by several mechanisms--bimolecular, Shockley-Read, or trap-limited. In the bimolecular process--for example, Auger or radiative recombination--when the radiation-induced excess carrier density is greater than the extrinsic carrier density $\Delta n > n_0$, the decay time constant decreases as the incident

TABLE II. PROMPT GAMMA DATA

Detector	n_0 (cm^{-3})	τ (ns)	ϵ_{ρ} (eV)
HRC	7×10^{14}	200	0.36
ADL	2.5×10^{14}	45	0.29
AF	8×10^{14}	240	0.43
HRC #8	10^{15}	250	0.37

⁹C. A. Klein, *J. Appl. Phys.*, 39 (1968), p. 2029.

¹⁰G. Nimtz, G. Bauer, R. Dornhaus, and K. H. Miller, *Phys. Rev. B*, 10 (1974), p. 3302.

radiation dose increases.¹¹ As the decay proceeds, eventually $\Delta n < n_0$ and the decay rate decreases approaching a limiting value.¹¹ When the decay takes place via defects located in the energy gap, the decay time constant in the high-excitation regime can be independent of excitation intensity depending on the number of defects and on the location of the defects on the energy gap. If the defect density n_t is small ($< n_0$) or if the defect energy coincides with the Fermi level and the number of excess electrons (Δn) equals the number of excess holes (Δp), then the decay proceeds exponentially via Shockley-Read recombination (see Blakemore,¹¹ page 259). If, however, some of the excited carriers are trapped at defects so that $\Delta n \neq \Delta p$, then the decay may not necessarily be characterized by a single exponential decay constant.¹² A longer decay constant can result, which will depend on the length of time the carriers are trapped at the defect sites and then re-emitted into the conduction band.

The decay curves for the AF and HRC #8 initially follow a bimolecular recombination process, with the decay time constant becoming shorter as the prompt gamma dose increases (see fig. 11 and 12). This occurred for doses > 1 rad, which, from equation (6), gives $n > 2 \times 10^{15} \text{ cm}^{-3}$ and is consistent with $\Delta n > n_0$. The value of the initial decay time constant at the lowest dose is 400 to 500 ns. This is the range for an Auger limited band-to-band recombination process (700 ns).¹³ The initial decay constants of the HRC (200 ns) and ADL (45 ns) are independent of dose and are shorter than those of the AF and HRC #8. This may be related to Shockley-Read recombination centers

¹¹J. S. Blakemore, *Semiconductor Statistics*, Pergamon Press, New York (1962), p. 209.

¹²R. A. Smith, *Semiconductors* Cambridge U. Press, Cambridge, MA (1959), p. 308.

¹³M. A. Kinch, M. J. Brau, and A. Simmons, *J. Appl. Phys.*, 44 (1973), p. 1649.

which shunt the bimolecular process. A low carrier concentration such as found for the ADL may be due to compensation and, hence, an increasing degree of Shockley-Read process recombination associated with it.¹² As the decay proceeds in the AF and HRC #8, an intermediate region with a dose-independent decay constant is observed for both detectors (fig. 13 and 14) equal to 1.3 and 0.67 μ s, respectively. Following this is a region with a decay constant equal to 5.5 μ s for both detectors. This longer time constant is probably due to a trapping level. The intermediate region could be due to either the tail of the bimolecular process or the onset of the trapping process.¹² As seen in figures 13 and 14, the decay characteristic follows a series of exponentials with various decay constants. It has been shown that if this is ascribable to a series of trapping processes, then the decay proceeds as $1/t^n$ where $n = 1$ for a uniform distribution of traps,¹⁴ or $n = 2$ when the traps are saturated at the beginning of the decay and the cross section of trapping equals the cross section for thermal emission.¹⁵ The data in figures 7 and 9 for AF indicate a $t^{-0.85}$ dependence from 0.1 to 20 μ s and are indicative of trapping processes. From figures 9, 13, and 14, the long-time response ($>10 \mu$ s) of ADL and HRC #8 are similar to that of the AF, indicating that the trapping mechanisms may be similar in these devices. It is noted that each of these detectors was fabricated by a different crystal growing procedure. The short-time response ($<1 \mu$ s), however, did show differences, especially for ADL as noted above.

¹²R. A. Smith, *Semiconductors* Cambridge U. Press, Cambridge, MA (1959), p. 308.

¹³M. A. Kinch, M. J. Brau, and A. Simmons, *J. Appl. Phys.*, 44 (1973), p. 1649.

¹⁴H. W. Leverenz, *An Introduction to Luminescence of Solids*, John Wiley and Sons, New York (1950), p. 270.

¹⁵R. H. Bube, *Photoconductivity of Solids*, John Wiley and Sons, New York (1960), p. 279.

It is difficult to determine the cause of the long decay time in the HRC detector. Since both the HRC and HRC #8 were fabricated by the same crystal growing procedure, it does not appear to be related to a material characteristic associated with the crystal growth. Long decay times (>milliseconds) are observed in $\text{Hg}_{0.8}\text{Cd}_{0.2}\text{Te}$; but under the experimental conditions of this experiment, two-carrier mode of operation is commonly observed. It is necessary to consider the detector response to luminescence produced by the ionizing radiation incident on detector substrate, windows, and surrounding material (e.g., glass). The HRC was mounted on a ZnS (IRTRAN II) substrate, whereas the AF and HRC #8 detectors were mounted on sapphire. The ZnS, as well as sapphire, is known to be luminescent material when exposed to ionizing radiation.^{16,17,18} But at doses considered here (300 rads), it is not expected to produce luminescence large enough to cause a significant detector response.¹⁷ Also, the ADL was mounted on a ZnS substrate and did not display a long decay tail. It is noted that the dewar windows of AF, HRC #8, and ADL (dome) were Ge, which is opaque to visible light, whereas the HRC had an IRTRAN II window, which transmits visible light. At present, however, it is not obvious how this would be responsible for the long decay tail. Finally, the HRC had a ZnS antireflection coating, whereas the surface of HRC #8 and ADL were untreated and the AF was passivated. The condition of the surface is known to be important to the operation of short-wavelength IR HgCdTe detectors in ionizing

¹⁶D. Curie, *Luminescence in Crystals*, Methuen, London (1963), p. 298.

¹⁷Radiation Effects in Passive Optical Sensor Components--Final Technical Report--SAMSO TR-74-19 LMSC-B324459 (December 1973); B. Passenheim, *Radiance and Attenuation of Luminescence in IR Detector Substrate Material*, Army Materials and Mechanics Research Center CTR-74-40 (June 1974).

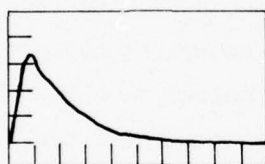
¹⁸L. P. Randolph, J. N. Lee, and R. B. Oswald, Jr., *IEEE Trans. Nucl. Sci.*, NS-22, No. 6 (1975), p. 2265.

radiation environments.¹⁹ Possibly the presence of the ZnS coating is responsible for the long decay tail in HRC, either through a direct coupling of the luminescence from the ZnS into the detector or through a surface-induced defect at the detector-coating interface.

6.2 Low-Level Gamma Counting

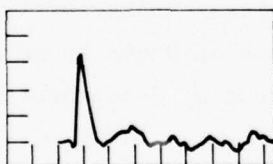
6.2.1 Data

Oscillograms of individual gamma pulses after being amplified ($\times 200$) are shown in figures 19 and 20 for the HRC and ADL detectors, respectively. Note that the decay time of HRC is



Horizontal scale: 100 ns/cm
Vertical scale: 200 mV/cm

Figure 19. Oscillogram of HRC response to single gamma event.



Horizontal scale: 100 ns/cm
Vertical scale: 20 mV/cm

Figure 20. Oscillogram of ADL response to single gamma event.

¹⁹*Proceedings of Meeting of IRIS Specialty Group on IR Detectors (July 1974): B. H. Breazeale, M. A. Kinch, and M. J. Brau, p. 295; M. M. Blouke and S. R. Borrello, p. 453; A. R. Chandua, B. L. Musicant, R. A. Rotolante, F. Junga, N. Nielsen, J. Pickel, S. Mims, and H. Nobel, p. 479.*

considerably longer than that of the ADL, similar to the prompt gamma response. The peak-pulse height of HRC is larger (by almost a factor of 10) than that for the ADL. Pulse-height distributions of these two detectors in a $2 \times 10^9 \text{ } \gamma/\text{cm}^2 \cdot \text{s}$ (1 rad/s) gamma field are shown in figures 21 and 22. The number of voltage pulses per second with an amplitude greater than some threshold P is plotted on semilog paper versus the threshold level. The dashed lines denote a trend of the data. The HRC detector was oriented with the optical axis parallel to the gamma field; the ADL was perpendicular to the field. Data were also taken on ADL with optical axis oriented 30 deg to the gamma field. Each orientation (of the ADL) gave nearly similar pulse-height distributions. The distributions of both detectors are exponential with the HRC exhibiting a smaller count rate than that of the ADL. Pulse-height distributions could not be measured on HRC #8 and AF.

6.2.2 Discussion and Comparison with Theory

An approximate value of the maximum voltage pulse induced by a single gamma--that is, secondary Compton gamma electron, calculated from equations (9) and (10)--is compared with the measured maximum (see fig. 21 and 22) in table III. The values of ϵ_0 were taken from table II and the value of $\Delta E/\Delta x = 10 \text{ MeV/cm}$ for CdTe^{20} was used in equation (10). Agreement within a factor of 3 to 4 is obtained for HRC and ADL, which is satisfactory for this approximate calculation. The values calculated for AF and HRC #8 are too small to be measured with our apparatus, as observed on these detectors.

²⁰H. L. Malm, T. W. Raudorf, M. Martini, and K. R. Zamo, *IEEE Trans. Nucl. Sci.*, NS-20, No. 1 (1973), 500.

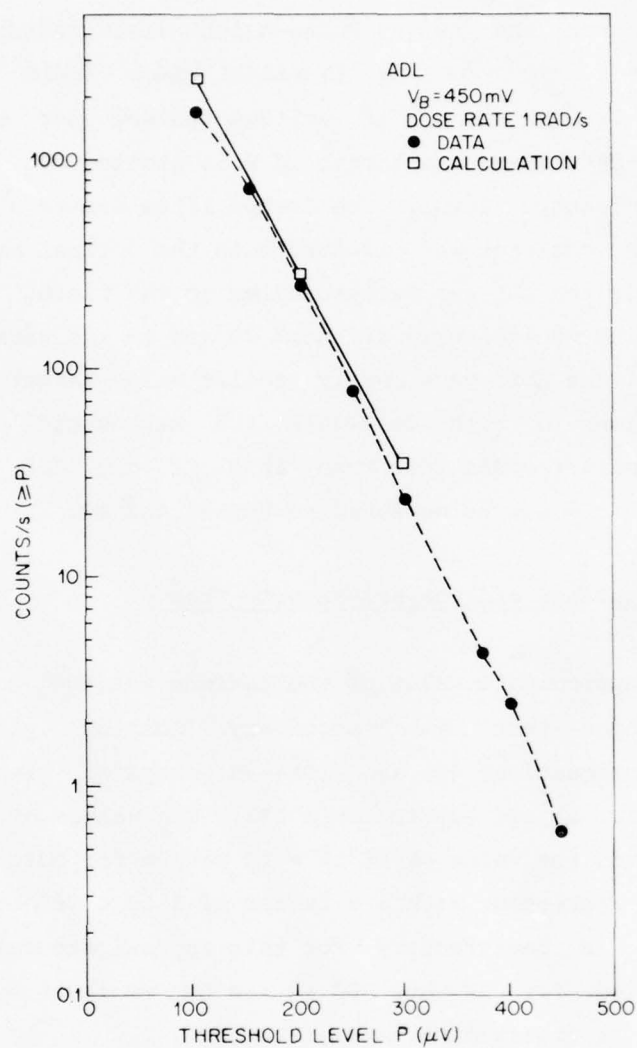


Figure 21. Pulse-height distribution for ADL in 1 rad/s gamma field.

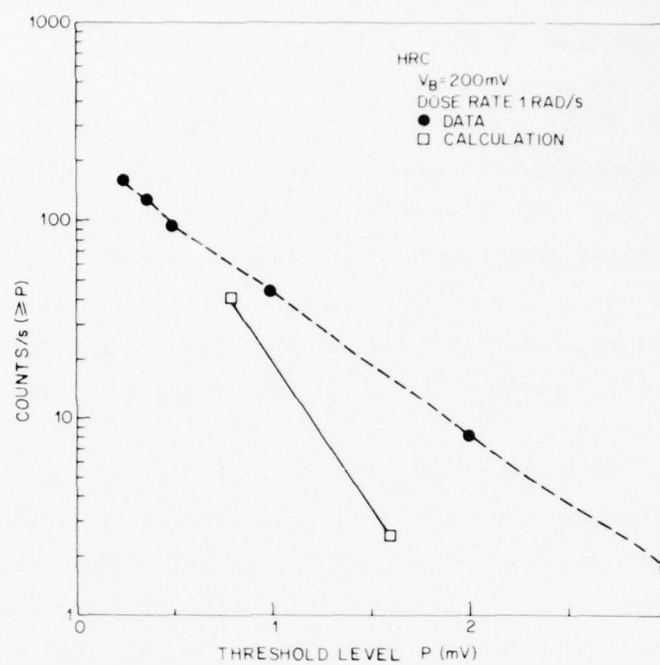


Figure 22. Pulse-height distribution for HRC in 1 rad/s gamma field.

TABLE III. LOW-LEVEL GAMMA-INDUCED PULSE HEIGHT

Detector	w_i (cm^2)	n_{O_2} (cm^{-3})	V_B (V)	Calculated V_p (μV)	Measured V_p (μV)
HRC	10^{-5}	$7 \cdot 10^{14}$	0.195	700	2000
ADL	$6.25 \cdot 10^{-14}$	$2.5 \cdot 10^{14}$	0.450	100	450
AF	$4.5 \cdot 10^{-3}$	$8 \cdot 10^{14}$	0.300	1.8	---
HRC #8	$6.25 \cdot 10^{-14}$	10^{15}	0.081	3.1	---

The maximum number of counts per second is larger than the value determined from internal events, $\dot{\gamma}_{\text{int}}$. For $\dot{\gamma} = 2 \times 10^9 \gamma/\text{cm}^2 \cdot \text{s}$ (1 rad/s), $\mu = 0.45 \text{ cm}^{-1}$ (taken from Malm et al.²⁰) (linear absorption coefficient of 1-MeV gamma in $\text{Hg}_{0.8}\text{Cd}_{0.2}\text{Te}$ based on a density of 7.5 g/cm^3) and the detector volumes, the calculated value is 12 counts/s for the HRC and 680 counts/s for the ADL detectors. This is considerably smaller than the largest measured value (see fig. 21 and 22) of 170 counts/s and 1700 counts/s, respectively, for the two detectors and is an indication that a portion of the pulses is due to Compton events originating external to the detector volume.

This is supported by the comparison of the measured pulse-height distribution with the calculated distribution (eq (11)) based on a contribution from external Compton events produced in the surrounding glass. Considering the approximations used in the calculation, good agreement between theory (solid line) and experiment (dashed line) is seen. These results were obtained by using the values of ϵ_p and n_o found in table II. Due to the isotropic penetrating nature of the radiation, the calculation also predicts no orientation dependence of the distribution, as observed. The agreement between the measured and calculated distribution is found to be better for the ADL detector than that found for the HRC detector. It is noted that the surface of the ADL was untreated, whereas the surface of the HRC had a ZnS coating. No account of surface treatment was taken in the calculation.

²⁰H. L. Malm, T. W. Raudorf, M. Martini, and K. R. Zamo, *IEEE Trans. Nucl. Sci.*, NS-20 (1973), 500.

6.3 High-Level Gamma Noise

6.3.1 Data

The rms gamma-induced noise voltage induced in the detector is plotted against dose rate (rads/s) for the four detectors in figures 23 to 26. The bandwidth of the voltage measurement is 4 MHz. The gamma-induced rms noise voltage V_Y was obtained from V_m , the rms voltmeter reading with the detector in the gamma field, and V_o , the reading with the detector out of the gamma field according to the following equation:

$$V_Y = \sqrt{V_m^2 - V_o^2} \quad (15)$$

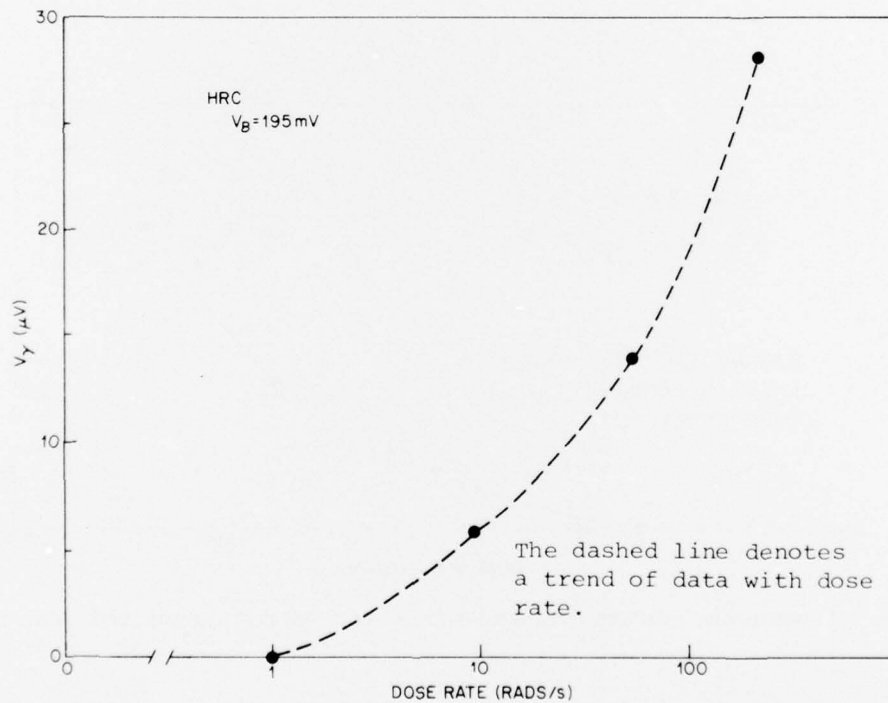


Figure 23. Gamma-induced noise versus dose rate for HRC.

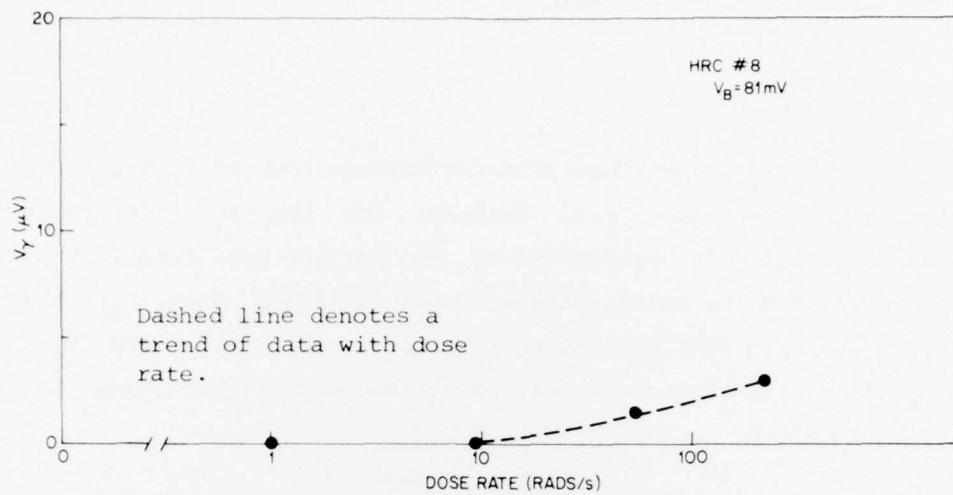


Figure 24. Gamma-induced noise versus dose rate for HRC #8.

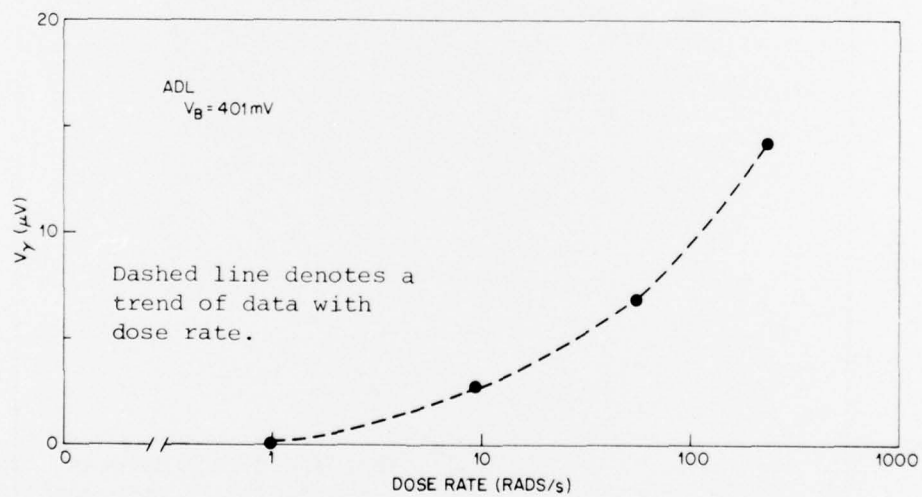


Figure 25. Gamma-induced noise versus dose rate for ADL.

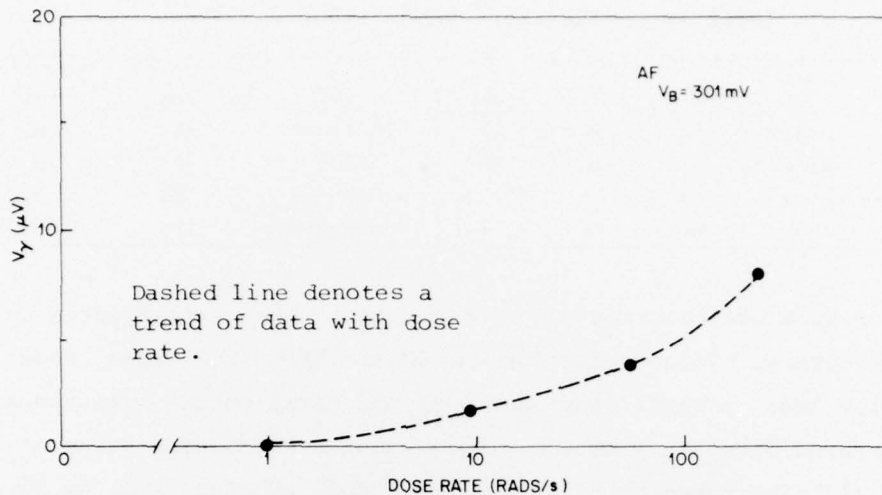


Figure 26. Gamma-induced noise versus dose rate for AF.

The value of V_o was easily obtained by lowering the ^{60}Co source into the pool after V_m was measured. The highest dose rate at which the measurement was performed was 220 rads/s. The largest noise voltage was induced in HRC, whereas the smallest was induced on HRC #8. Since many detector applications require operation at reduced bandwidth, the measurement was performed with a 420-Hz filter in the circuit. This had the effect of reducing the radiation-induced noise below the sensitivity of the measurement for all detectors except for the HRC, which gave a value of 1 μV .

6.3.2 Comparison of Theory and Experiments

The experimental values of the rms gamma-induced noise measured at 220 rads/s are compared in table IV with the theoretical values, based on equation (12). The values of V_p were taken from the calculated values in table III (eq (9) and (10)), by using ϵ_p from the prompt gamma experiments (table II). The values of τ for HRC and ADL

TABLE IV. HIGH-LEVEL GAMMA-INDUCED NOISE

Detector	wtd (cm ³)	τ (ns)	K	V_P (μ V)	B (Hz)	Calculated V_Y (μ V)	Measured V_Y (μ V)
HRC	1.2×10^{-8}	150	20	700	$1/2\pi\tau = 1.06 \times 10^6$	65	28
ADL	7.5×10^{-7}	20	10	90	$\Delta f = 4 \times 10^6$	15	14
AF	1.1×10^{-5}	520	10	1.8	$1/2\pi\tau = 0.3 \times 10^6$	6.8	8.0
HRC #8	7.5×10^{-7}	420	10	3.1	$1/2\pi\tau = 0.37 \times 10^6$	2.8	2.9

were taken from oscillograms of single gamma events in figures 19 and 20, respectively. Values of τ for HRC #8 and AF were taken from the initial low dose prompt gamma data, as the gamma pulses were too small to be measured directly from the single gamma events. The value of K in equation (13) was taken to be 20 for HRC and 10 for ADL, based on a comparison of the extrapolation of the count rate to zero pulse height in the experimental pulse height distribution (fig. 21 and 22) with the calculated internal event rate; K was taken to be 10 for AF and HRC #8. Considering the number of parameters in the calculation, there is very good agreement between theory and experiment for all the detectors even with the factor-of-two difference for HRC. Reducing the bandwidth to 420 Hz predicts a value of V_Y equal to 1.3 μ V for the HRC at 220 rads/s. The measured value was 1 μ V.

7. CONCLUSIONS

The results of these experiments--prompt gamma, low-level counting and high-level gamma-induced noise--indicate that the average value of the electron-hole pair creation energy ϵ_p of $\text{Hg}_{0.8}\text{Cd}_{0.2}\text{Te}$ is 0.36 ± 0.07 eV. This is consistent with the value predicted by Klein.⁹ Analysis of gamma-counting and noise experiments indicates that

⁹C. A. Klein, *J. Appl. Phys.*, 39 (1968), p. 2029.

the majority of the gamma events originates from Compton interactions in the surrounding material--for example glass dewar external to the detector. Initial decay characteristics of the detector response following a prompt gamma pulse appear to depend on the detector material, proceeding either through a bimolecular or a Shockley-Read recombination process. At longer times, trap-limited processes become operative in which the fractional level of decay reaches the same value of all the material-preparation techniques evaluated. This applies to detectors in which the surface was left untreated or was passivated. A detector with the surface treated with a ZnS antireflection coating, however, exhibited an enhanced long time decay response at the largest gamma doses.

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LITERATURE CITED

- (1) C. Harman, J. Electronic Mat., 1, (1972). p. 230.
- (2) J. Steininger, Proceedings of Meeting of IRIS Specialty Group on IR Detectors (13-15 March 1973) p. 33.
- (3) P. W. Kruse, Appl. Optics, 4 (1965), p. 687.
- (4) R. A. Rotolante, R. P. Muroska, and G. E. Keiser, Radiation Effects in Intrinsic Photodetector Systems (U), Honeywell Radiation Center AMMRC CTR 73-46 (December 1973). (SECRET)
- (5) J. W. Haffner, Presented at 1975 IEEE, Annual Conference Nuclear and Space Radiation Effects, Poster Session Paper (14-17 July 1975).
- (6) Detector Test Program Final Report, Vol. 1, LMSC-B303910 Contract FO4701-70-C-0227 (August 1972).
- (7) J. C. Pickel and M. D. Petroff, IEEE Trans. Nucl. Sci., NS-22, No. 6 (1975), p. 2456.
- (8) D. Long and J. L. Schmitt, Mercury-Cadmium Telluride and Closely Related Alloys, Semiconductors and Semimetals, Vol. 5, ed. by R. K. Willardson and A. C. Beer, Academic Press, New York (1970), p. 175.
- (9) C. A. Klein, J. Appl. Phys., 39 (1968), p. 2029.
- (10) G. Nimtz, G. Bauer, R. Dornhaus, and K. H. Miller, Phys. Rev. B, 10 (1974), p. 3302.
- (11) J. S. Blakemore, Semiconductor Statistics, Pergamon Press, New York (1962), p. 209.
- (12) R. A. Smith, Semiconductors, Cambridge U. Press, Cambridge, MA (1959), p. 308.
- (13) M. A. Kinch, M. J. Brau, and A. Simmons, J. Appl. Phys., 44 (1973), p. 1649.
- (14) H. W. Leverenz, An Introduction to Luminescence of Solids, John Wiley and Sons, New York (1950), p. 270.

LITERATURE CITED (CONT'D)

- (15) R. H. Bube, Photoconductivity of Solids, John Wiley and Sons, New York (1960), p. 279.
- (16) D. Curie, Luminescence in Crystals, Methuen, London (1963), p. 298.
- (17) Radiation Effects in Passive Optical Sensor Components--Final Technical Report--SAMSO TR-74-19 LMSC-B324459 (December 1973); B. Passenheim, Radiance and Attenuation of Luminescence in IR Detector Substrate Material, Army Materials and Mechanics Research Center CTR-74-40 (June 1974).
- (18) L. P. Randolph, J. N. Lee, and R. B. Oswald, Jr., IEEE Trans. Nucl. Sci., NS-22, No. 6 (1975), p. 2265.
- (19) Proceedings of Meeting of IRIS Specialty Group on IR Detectors (July 1974): B. H. Breazeale, M. A. Kinch, and M. J. Brau, p. 295; M. M. Blouke and S. R. Borrello, p. 453; A. R. Chandua, B. L. Musicant, R. A. Rotolante, F. Junga, N. Nielsen, J. Pickel, S. Mims, and H. Nobel, p. 479.
- (20) H. L. Malm, T. W. Raudorf, M. Martini, and K. R. Zamo, IEEE Trans. Nucl. Sci., NS-20 No. 1 (1973), p. 500.

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